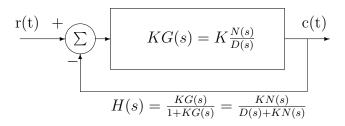
## Nyquist Criterion For Stability of Closed Loop System

Prof. N. Puri ECE Department, Rutgers University

## 1 Nyquist Theorem

Given a closed loop system:



- *n*: The order of denominator polynomial D(s);
- KG(s) =Open Loop Transfer Function;
- $D(S) = \text{Open Loop Characteristic polynomial with } \mathbf{O}$  unstable roots (unstable open loop poles) and  $n \mathbf{O}$  stable roots;
- P(s) = D(s) + KN(s) = Closed Loop Characteristic polynomial with C unstable roots (unstable closed loop poles);
- $KG(j\omega) =$ Open Loop frequency response;
- $1 + KG(j\omega) =$  Shifted Plot.

The plot of  $(1 + KG(j\omega))$  as  $\omega$  varies from  $\omega = -\infty$  to  $\omega = \infty$  is referred to as "Nyquist Locus" in  $(1 + KG(j\omega))$  plane. Plot of Nyquist Locus in  $(1 + KG(j\omega))$  plane determines the stability of the Closed Loop System. Let

 $\mathbf{N}$  = number of counter clockwise encirclements of the origin (0 + 0j) by the Nyquist Locus as  $\omega$  varies from  $-\infty$  to  $\infty$ , in  $(1 + KG(j\omega))$  plane.

Nyquist Theorem state:

$$\mathbf{N} = \mathbf{O} - \mathbf{C} \tag{1}$$

So this implies:

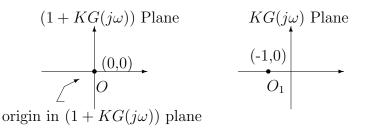
• if  $\mathbf{C} = 0$ , the conclusion is:

Feedback control system is stable, if the number of counterclockwise encirclements of the origin in  $(1 + KG(j\omega))$  plane is equal to the number of open loop unstable poles **O**.

• if  $\mathbf{O} = 0$  and  $\mathbf{C} = 0$ , the conclusion is:

Feedback control system is stable if the Nyquist Locus in  $(1 + KG(j\omega))$  does not encircle the origin.

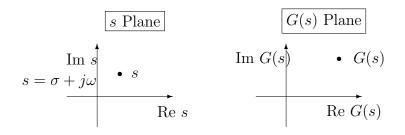
Origin in  $(1 + KG(j\omega))$  transform to -1 + j0 point in  $KG(j\omega)$  plane.



 $O_1(0,0)$  in  $(1 + KG(j\omega))$  plane is "Mapped" into  $O_1(-1,0)$  in  $KG(j\omega)$  plane, the point  $O_1$  is referred to as the critical point.

## **2** Graphical Interpretation of G(s)

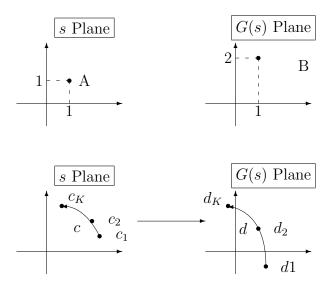
• Concept of G(s) as a "Mapping" form s plane to G(s) plane.



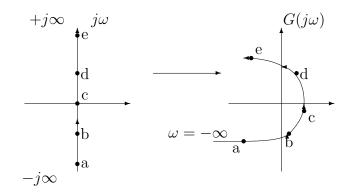
A point s in s plane is "Mapped" into a point G(s) in G(s) plane. Example: Consider function  $G(s) = 1 + s^2$ , when s = 1 + j, then

$$G(s) = 1 + s^{2} = 1 + (1 + j)^{2} = 1 + 1 + (-1) + 2j = 1 + 2j$$

Point A in s plane has been mapped in B in G(s) plane. Let s be moving on a curve c as  $c_1, c_2, \dots, c_K$ , then corresponding points move in G(s) plane along  $d_1, d_2, \dots, d_K$ . Thus the curve c in s plane has been mapped to curve d in G(s) plane via the function G(s).



•  $G(s)|_{s=j\omega} = G(j\omega)$  implies that s is allowed to take values only in the imaginary axis of the s plane. Thus as  $\omega$  is varied from  $\omega = -\infty$  to  $\omega = +\infty$ , the whole of the  $j\omega$  axis in the s plane is mapped into a locus in the  $G(j\omega)$  plane.



•  $G(j\omega)$  can be considered as a phaser.

$$G(j\omega) \text{ Plane}$$

$$X(\omega) \qquad \qquad G(j\omega)$$

$$A(\omega) \qquad \qquad G(j\omega) = R(\omega) + jX(\omega)$$

$$R(\omega)$$

$$G(j\omega) = R(\omega) + jX(\omega) = \left[R^2(\omega) + X^2(\omega)\right]^{\frac{1}{2}} \angle \tan^{-1}\frac{X(\omega)}{R(\omega)} = A(\omega)\angle\varphi(\omega)$$

And it has the following properties. If given  $G_1(j\omega)$ ,  $G_2(j\omega)$  as

$$G_1(j\omega) = A_1(\omega) \angle \varphi_1(\omega) = R_1(\omega) + jX_1(\omega)$$
  

$$G_2(j\omega) = A_2(\omega) \angle \varphi_2(\omega) = R_2(\omega) + jX_2(\omega)$$

then

$$G_{1}(j\omega) + G_{2}(j\omega) = [R_{1}(\omega) + R_{2}(\omega)] + j [X_{1}(\omega) + X_{2}(\omega)]$$
  

$$G_{1}(j\omega)G_{2}(j\omega) = A_{1}(\omega)A_{2}(\omega)\angle [\varphi_{1}\omega + \varphi_{2}(\omega)]$$
  

$$\frac{G_{1}(j\omega)}{G_{2}(j\omega)} = \frac{A_{1}(\omega)}{A_{2}(\omega)}\angle [\varphi_{1}\omega - \varphi_{2}(\omega)]$$

## **3** Proof of Nyquist Criterion

Restate the theorem here:

Given:

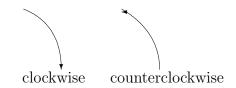
- KG(s) =Open Loop Transfer Function with **O** unstable poles;
- $H(s) = \frac{KG(s)}{1+KG(s)}$  = Closed Loop Transfer Function with **C** unstable poles;
- N = number of counterclockwise encirclements of (-1+j0) point by the locus of  $G(j\omega)$ ,  $-\infty < \omega < +\infty$ ;
- n = degree of D(s).

Nyquist Theorem states that:

$$\mathbf{C} = -\mathbf{N} + \mathbf{O},$$

and  $\mathbf{C} = 0$  implies stability of the closed loop system.

This implies that "For a system to be closed loop stable, the number of encirclements of (-1 + j0) point by the locus of  $G(j\omega)$ ,  $-\infty < \omega < +\infty$  in the counterclockwise direction is equal to the number of unstable open loop poles."



Proof:

$$F(s) = 1 + KG(s) = 1 + \frac{KN(s)}{D(s)} = \frac{D(s) + KN(s)}{D(s)} = \frac{P(s)}{D(s)}$$
$$F(s) = \frac{\prod_{i=1}^{n} (s - p_{ic})}{\prod_{k=1}^{n} (s - p_{ko})}, \quad F(j\omega) = \frac{\prod_{i=1}^{n} (j\omega - p_{ic})}{\prod_{k=1}^{n} (j\omega - p_{ko})}$$

$$F(j\omega) = |F(j\omega)| \angle \varphi_F(\omega), \quad \varphi_F(\omega) = \sum_{i=1}^n \varphi_{ic}(\omega) - \sum_{k=1}^n \varphi_{ko}(\omega)$$

$$\Delta \varphi_F(\omega)|_{\omega=-\infty}^{+\infty} = \sum_{i=1}^n \Delta \varphi_{ic}(\omega)|_{\omega=-\infty}^{+\infty} - \sum_{k=1}^n \Delta \varphi_{ko}(\omega)|_{\omega=-\infty}^{+\infty}$$

$$\frac{s \text{ Plane}}{\sum_{i=1}^{n} \Delta \varphi_{ic}(\omega)|_{\omega=-\infty}^{+\infty}} - \sum_{k=1}^n \Delta \varphi_{ko}(\omega)|_{\omega=-\infty}^{+\infty}$$

$$S \text{ Plane}$$

$$L.H.S. \qquad s \text{ Plane}$$

$$L.H.S. \qquad s \text{ Plane}$$

$$L.H.S. \qquad j \omega - p$$

$$j \omega - p$$

then

Then for  $F(s) = \frac{D(s)+KN(s)}{D(s)}$ , it has *n* zeros and *n* poles. And it has zeros which are same as Closed Loop poles and has poles which are same as open loop poles. Now

$$F(s) \text{ has } \begin{cases} (n - \mathbf{C}) \text{ zeros in L.H.S. and } \mathbf{C} \text{ zeros in R.H.S.} \\ (n - \mathbf{O}) \text{ poles in L.H.S. and } \mathbf{O} \text{ poles in R.H.S.} \end{cases}$$

Thus

$$\Delta \varphi_F(\omega)|_{\omega=-\infty}^{+\infty} = \sum_{i=1}^n \Delta \varphi_{ic}(\omega)|_{\omega=-\infty}^{+\infty} - \sum_{k=1}^n \Delta \varphi_{ko}(\omega)|_{\omega=-\infty}^{+\infty}$$
$$= [\pi(n-\mathbf{C}) - \pi\mathbf{C}] - [\pi(n-\mathbf{O}) - \pi\mathbf{O}] = -2\pi(\mathbf{C}-\mathbf{O}) = 2\pi N \quad (2)$$

where

N = counterclockwise encirclements of origin in  $(1 + G(j\omega))$  plane = counterclockwise encirclements of (-1 + j0) in  $G(j\omega)$  plane